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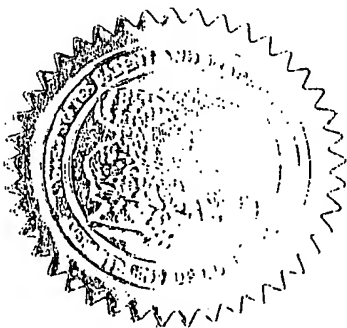
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**PROVISIONAL APPLICATION FOR PATENT COVER SHEET**

This is a request for filing a PROVISIONAL APPLICATION FOR PATENT under 37 CFR 1.53 (b)(2).

Docket Number

28988

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**TITLE OF THE INVENTION (280 characters max)****ELECTROMAGNETIC SENSORS FOR TISSUE CHARACTERIZATION****CORRESPONDENCE ADDRESS**

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**ENCLOSED APPLICATION PARTS (check all that apply)**

<input checked="" type="checkbox"/> 18 pages of specification (including Abstract page)	<input checked="" type="checkbox"/> 22 Claims
<input checked="" type="checkbox"/> 11 sheets of drawings	<input checked="" type="checkbox"/> Applicant is entitled to Small Entity Status under 37 CFR 1.9 and 37 CFR 1.27
<input checked="" type="checkbox"/> 29 total pages	

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Provisional Application Filing Fee	1	\$ 100		\$ 200
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☒ No ☐ Yes, the name of the US Government agency and the Government contract number are: \_\_\_\_\_

Respectfully submitted,

SIGNATURE Martin D. Moynihan

29 March 2005

Date

40,338

REGISTRATION NO.  
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TYPED or PRINTED NAME Martin Moynihan

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**APPLICATION FOR PATENT**

Inventors: Dan HASHIMSHONY, Gil COHEN, and Iddo GELTNER

Title: Electromagnetic Sensors For Tissue Characterization

**FIELD AND BACKGROUND OF THE INVENTION**

The present invention relates to a method and apparatus for tissue characterization, by resonance of reflected electromagnetic wave signals.

Tissue characterization by its electromagnetic reflective properties, for differentiating between tissue types, is known. In general it involves the propagation of an electromagnetic wave at about the microwave range, in a coaxial cable, from an electromagnetic-wave generator to the tissue to be characterized. At the proximal end with respect to the tissue, the coaxial cable may be cut and brought in contact with the tissue. Alternatively, various geometries may be provided, as coaxial endings, operative as a tissue probes.

For example Burdette, et al. [Burdette et al, "In Vivo Probe Measurement Technique for Determining Dielectric Properties at VFW Through Microwave Frequencies", IEEE Trans. On Microwave Theory & Techniques, MTT-28 (4): 414-427, 1980] describe theoretically and experimentally the use of a probe technique in order to determine the dielectric properties of semisolid material and living tissue, in situ. This method is advantageous compared to previous methods known by the following:

1. enabling measurements of the dielectric properties in living tissue in a continuous frequency range of between about 0.1 GHz and about 10 GHz,
2. eliminating the need for tedious sample preparation, and
3. enabling data processing on a real-time basis.

The Burdette idea is to use a short monopole antenna, suitable for insertion into living tissues, as the in vivo probe. The probe is designed as a coaxial cable having an outer and an inner (center) conductor separated by a Teflon dielectric

material. The inner conductor cable is slightly longer than the outer one in order to create an electric field of a monopole at the distal tip with respect to operator. This tip is to be inserted into the tissue, which dielectric properties are to be measured. The outer conductor may be grounded for minimizing fringe effects. An SMA connector is attached to the probe by first removing the inner conductor and the Teflon dielectric material, soldering it to the outer conductor and then reassembling the probe with the center conductor as the center pin of the connector. While disassembled, the probe conductors are flashed with nickel plating and then plated with gold in order to reduce chemical reactions between the probe and the electrolyte within the tissue to be examined. This process virtually eliminates oxidation of the probes metallic surfaces and helps minimize electrode polarization effects at lower frequencies.

US Patent 5,744,971, to Chan et al., teaches the use of a coaxial probe for measuring the dielectric properties of materials suitable, although not exclusively so, for the use in the non-invasive monitoring of the conservation treatment of cultural material e.g. works of art such as canvas. The probe is a needle like device with the coaxial structure extending to the distal tip with respect to the operator. The probe is extracorporeal as opposed to the invasive probe of Burdette. The design of this coaxial probe differs slightly from the one of Burdette et al.

US Patent 6,026,323, to Skladnev et al. describes a probe to characterize tissue types that combines optical and electrical tests in a single device, capable of providing the optical and electrical data almost simultaneously from very small areas of a tissue surface. Key to this approach is an instrument capable of making almost simultaneous electrical and optical measurements on the same small areas of tissue. Each measurement involves a complex sequence of events which includes: optical and electrical tissue stimulations with subsequent detection, filtering and digitization of the tissue response; extraction of specific parameters from the optical and electrical signals; checking for errors, and subsequent classification of the extracted parameters into various tissue type categories; and feedback to the system operator. The probe has a central optical fiber, which conducts electromagnetic radiation to a photo-detector diode in the handle and is positioned in the center of a bundle of optical fibers all of which are located within an external tube. A three gold electrodes are positioned adjacent and abutting against the internal surface of the external tube. The probe cable consists many individual coaxial conductors with a single overall braided

shield, enclosed in a medically rated silicone outer jacket. Both ends of the cable have round plastic pin male connectors. The electrodes and optical fibers come into direct contact with the tissue for stimulation and detection of the tissue characteristics. The probe tip is polished and smoothed and has contoured edges. An epoxy resin electrically insulates and seals the tip section.

US Patent 6,813,515 to Hashimshony teaches a probe, method and system for examining tissue, in order to differentiate it from other tissue, according to its dielectric properties. The method is of generating an electrical fringe field in the examined tissue to produce a reflected pulse therefrom with negligible radiation penetrating into the tissue itself; detecting the reflected electrical pulse; and comparing electrical characteristics of the reflected electrical pulse with respect to the applied electrical pulse to provide an indication of the dielectric properties of the examined tissue. The measuring device is built as a coaxial probe with cavity at its distal tip with respect to operator where a sample of the tissue to be examined is confined. The probe itself has an inner conductor insulated from, and enclosed by, an outer conductor open at one end and extending past the inner conductor in the axial direction, defining an open cavity at the distal end of the probe with respect to the operator. The inner conductor includes a tip within the open cavity, which tip is formed with at least two different diameters for enhancing the electrical fringe field.

US Patent 6,370,426, to Campbel et al., describes a method and apparatus for measuring relative hydration of a substrate. Measurements of the electrical characteristics of the substrate, the force applied to it, and the temperature of the substrate during the measurement provide inputs for determining such relative hydration of the substrate. The structure of the sensor used in this case is of two coaxial conductors one of which runs along the axis of symmetry, separated by a coaxial insulator and having a coaxial insulator outside the outer conductor. Both conductors and the separating insulator end at a plane perpendicular to the axis of symmetry at the distal tip with respect to the operator, so that the coaxial structure comes to contact with the examined tissue but does not penetrate it.

British Patent GB01153980, to Einat et al., describes an RF antenna, operative as a probe for near field identification and characterization. It has first and second radiative portions, generating electromagnetic fields, which are substantially

opposing, so as to suppress far field radiation. The far-field suppression minimizes contribution from the far field, when near field characterization is sought.

Unlike the aforementioned systems, of tissue characterization by its electromagnetic reflective properties, US Patent 5,227,730, to King, et al., adds an element of resonance. King et al., teach a method and apparatus for sensing complex dielectric properties of lossy (dissipative) dielectric materials in vivo or in vitro, particularly biological tissue. This idea is based on a needle-like resonant sensor, which is inserted into the test material for measuring its dielectric properties at the resonant frequency. The major advantage, compared to the sensors described hereinabove, is that due to the resonating effect, the dielectric constants can be measured with a greater accuracy and resolution, and over a much larger volume (of the order of a cubic centimeter). Thus, the resonant sensor is able to better distinguish between tumors and normal tissue. The needle-like resonant sensor, as designed by King, et al., has the form of a dipole resonator that is positioned parallel and adjacent to a miniature coaxial feed cable and is electrically insulated from it. The dipole resonator is inductively coupled to the microwave power in the coaxial cable by means of an electrically short circumferential gap cut in the cable shield. By coupling the gap to the dipole at its center currents are induced in the dipole in a perfectly balanced and symmetric manner. With proper design of the feed gap, the dipole impedance can be well matched to the coaxial cable with very small reflection from the gap at the resonant frequency of the dipole. To regulate the degree of coupling between the dipole and the test medium, a thin cylindrical dielectric sheath encloses the entire assembly. Such a sheath might be, for example, a dielectric catheter into which the coaxial cable with its attached dipole resonator is inserted.

Except for the device of King et al., the systems described hereinabove are non-resonating, so the differences between signals from different tissue types are small, while the device of King, et al. is invasive.

A probe for tissue characterization with greater versatility would be desirable.

### **SUMMARY OF THE INVENTION**

The present invention is of a sensor for tissue characterization, comprising: a resonating element, formed as a conductive structure, configured to be placed proximally to an edge of a tissue for characterization, without penetrating the tissue, and having a diameter-equivalent  $D$ , which defines a cross-sectional area of the resonating element, on a plane substantially parallel with the edge; and at least one conductive lead, for providing communication with an external system, wherein the resonating element is configured to resonate at a free-air wavelength range of between about  $\lambda$  and about  $10\lambda$ , wherein  $\lambda$  is at least about ten times the diameter-equivalent  $D$ , and wherein upon receiving a signal in the range of between about  $\lambda$  and about  $10\lambda$ , the sensor is configured to induce electric and magnetic fields, in a near zone, in the tissue, the near zone being a hemisphere having a diameter of substantially  $D$ , beginning with the edge, while causing negligible radiation in a far zone, so that the tissue, in the near zone, effectively functions as part of the resonating element, varying a resonating response to the sensor, and so the tissue, in the near zone, is thereby characterized by its electromagnetic properties, by the resonating response to the sensor.

Unless otherwise defined, all technical and scientific terms used herein have the same meaning as commonly understood by one of ordinary skill in the art to which this invention belongs. Although methods and materials similar or equivalent to those described herein can be used in the practice or testing of the present invention, suitable methods and materials are described below. In case of conflict, the patent specification, including definitions, will control. In addition, the materials, methods, and examples are illustrative only and not intended to be limiting.

### **BRIEF DESCRIPTION OF THE DRAWINGS**

The invention is herein described, by way of example only, with reference to the accompanying drawings. With specific reference now to the drawings in detail, it is stressed that the particulars shown are by way of example and for purposes of illustrative discussion of the preferred embodiments of the present invention only, and are presented in the cause of providing what is believed to be the most useful and readily understood description of the principles and conceptual aspects of the invention. In this regard, no attempt is made to show structural details of the invention



in more detail than is necessary for a fundamental understanding of the invention, the description taken with the drawings making apparent to those skilled in the art how the several forms of the invention may be embodied in practice.

In the drawings:

5        Figures 1 schematically illustrates a system and a sensor for tissue characterization, in accordance with the present invention;

      Figures 2A – 2B schematically illustrate schematic circuits for the sensor for tissue characterization, in accordance with the present invention;

10       Figures 3A – 3K schematically illustrate various geometries for the resonating elements of the sensor for tissue characterization, in accordance with the present invention;

      Figures 4A – 4C schematically illustrate the sensor for tissue characterization, formed as a thin, flexible construction, in accordance with an embodiment of the present invention;

15       Figures 5A – 5G schematically illustrate the sensor for tissue characterization operative with a housing, in accordance with the present invention;

      Figures 6A – 6C schematically illustrate various manners of combining spiral and a helix, in accordance with the present invention; and

20       Figure 7 schematically illustrates experimental data, of the sensor for tissue characterization of the present invention.

#### **DESCRIPTION OF THE PREFERRED EMBODIMENTS**

      The present invention is of a sensor for tissue characterization, comprising: a resonating element, formed as a conductive structure, configured to be placed  
25       proximally to an edge of a tissue for characterization, without penetrating the tissue, and having a diameter-equivalent  $D$ , which defines a cross-sectional area of the resonating element, on a plane substantially parallel with the edge; and at least one conductive lead, for providing communication with an external system, wherein the resonating element is configured to resonate at a free-air wavelength range of between  
30       about  $\lambda$  and about  $10\lambda$ , wherein  $\lambda$  is at least about ten times the diameter-equivalent  $D$ , and wherein upon receiving a signal in the range of between about  $\lambda$  and about  $10\lambda$ , the sensor is configured to induce electric and magnetic fields, in a near zone, in the tissue, the near zone being a hemisphere having a diameter of substantially  $D$ ,

beginning with the edge, while causing negligible radiation in a far zone, so that the tissue, in the near zone, effectively functions as part of the resonating element, varying a resonating response to the sensor, and so the tissue, in the near zone, is thereby characterized by its electromagnetic properties, by the resonating response to the sensor.

Before explaining at least one embodiment of the invention in detail, it is to be understood that the invention is not limited in its application to the details of construction and the arrangement of the components set forth in the following description or illustrated in the drawings. The invention is capable of other embodiments or of being practiced or carried out in various ways. Also, it is to be understood that the phraseology and terminology employed herein is for the purpose of description and should not be regarded as limiting.

Referring now to the drawings, Figure 1 schematically illustrates a system 10, having a sensor 20 for tissue characterization, in accordance with the present invention.

The sensor 20 has proximal and distal ends, 21 and 29, with respect to a tissue 18, which is the tissue to be characterized.

The sensor 20 includes a resonating element 42, formed as a conductive structure, configured to be placed proximally to an edge 13 of the tissue 18 for characterization, while in air 16, that is, without penetrating the tissue 18.

The resonating element 42 has a diameter-equivalent  $D$ , which defines a cross-sectional area on a side of the edge 13, substantially parallel with the edge 13. Preferably,  $D$  is between about 3 mm and 25 mm. It will be appreciated that other values, which are larger or smaller, may similarly be used.

Additionally, the resonating element 42 is associated with a circuit 40, by resistance coupling or by inductive coupling. The circuit 40 communicates with an external signal-generation-control-and-analysis system 30, via a coupler 50 and a transmission line, for example, a coaxial cable 56.

The resonating element 42 is configured to resonate at a free-air wavelength range of between about  $\lambda$  and about  $10\lambda$ , wherein  $\lambda$  is at least about ten times the diameter-equivalent  $D$ . Thus, the free-air wavelength range of between about  $\lambda$  and about  $10\lambda$  is generally equivalent to a frequency range of between about 10 Mhz and about 5 Ghz,

Upon receiving a signal in the range of between about  $\lambda$  and about  $10\lambda$ , the resonating element 42 is configured to induce an electric field 12 and a magnetic field 14, in a near zone 17 of the tissue 18, wherein the electric field 12 penetrates the tissue 18 to a depth of  $D(E)$  and the magnetic field 14 penetrates the tissue 18 to a depth of  $D(B)$ , both being of the order of magnitude of  $D$ . Preferably,  $D(B)$  is somewhat larger than  $D(E)$ , for example, by a factor of between 1.1 and 5. Alternatively, they are substantially the same. However, it will be appreciated that in some cases,  $D(B)$  may be smaller than  $D(E)$ .

Thus, the region of penetration of  $D(B)$  and  $D(E)$  is a hemisphere 15 of a diameter  $R$ , which is substantially equivalent to  $D$ , and which begins with the tissue edge 13. The tissue 18, in the hemisphere 15, effectively functions as part of the resonating element 42, varying its resonating response. In consequence, the tissue 18, in the hemisphere 15, may be characterized based on its electromagnetic properties, by its resonating response.

Additionally, the resonating element 42 is configured as an inefficient antenna, for the free-air wavelength range of between about  $\lambda$  and about  $10\lambda$ , so its radiation efficiency in a far zone 19 is less than 0.1% and preferably less than 0.01%. As a result, contributions of the far zone are minimized and the tissue characterization is limited to the hemisphere 15 of the near zone 17, very close to the edge 13.

The effect is similar to that achieved by British Patent GB01153980, to Einat et al., which describes an RF antenna, operative as a probe for near field identification and characterization. It has first and second radiative portions, generating electromagnetic fields, which are substantially opposing, so as to suppress far field radiation. The far-field suppression minimizes contribution from the far field, when near field characterization is sought.

The external signal-generation-control-and-analysis system 30 preferably includes a signal generator 32, an analyzer 34, and a controller 36, although these may be integrated into a single unit. A user interface may be provided, for example, in the form of read and write drives 31, such as, a diskette, a CD, a DVD, a disk-on-key and the like, for providing predetermined operating parameters and settings, and in order to store test results. A display screen 38 may display the resonating response. It will be appreciated that other output means, for example, a printer or a facsimile, are also possible. A keyboard 35 may be used to input data such as patient details, date and

time of a particular test, signal parameters, and the like. Additionally, the controller 36 may include other input and output devices, for example, a USB port 33, and other features, as known.

Referring further to the drawings, Figures 2A and 2B illustrate schematic circuits of the sensor 20, in accordance with the present invention.

As seen in Figure 2A, the sensor 20 may be represented as a circuit 40, which includes the resonating element 42, configured to be placed proximally to the tissue 18. Additionally, the circuit 40 may include an effective component 44, having an effective resistance, an effective inductance, and an effective capacitance, and which may be connected in series with the resonating element 42, and an effective component 46, having an effective resistance, an effective inductance, and an effective capacitance, and which may be connected in parallel with the resonating element 42.

The coupler 50 preferably includes a connection structure 52, which preferably provides at least one of tuning, switching, and replacing capabilities, for example, in order to change the overall impedance of the circuit 40, or of the components 44 and 46. These capabilities may be desired to interchangeably optimize the sensor 20 for characterizing different types of tissue, for example, breast tissue, which is predominantly fat, muscle tissue, skin tissue, and bone.

A connector 54 connects the connection structure 52 and the transmission line 56, preferably, while ensuring impedance matching and balancing.

As seen in Figure 2B, the sensor 20 may be represented as two circuits 40A and 40B, which include two resonating elements 42A and 42B, connected in parallel. Additionally, the circuits 40A and 40B may include effective components 44A and 44B, each having an effective resistance, an effective inductance, and an effective capacitance, and which may be connected in series with the resonating elements 42A and 42B, and effective components 46A and 46B, each having an effective resistance, an effective inductance, and an effective capacitance, and which may be connected in parallel with the resonating elements 42A and 42B.

Additionally, the two circuits 40A and 40B may be associated with connection structures 52A and 52B, which preferably provide at least one of tuning, switching, and replacing capabilities to the circuits 42A and 42B.

The connector 54 connects the connection structures 52A and 52B and the transmission line 56, preferably, while ensuring impedance matching and balancing.

Referring further to the drawings, Figures 3A – 3K schematically illustrate various geometries for the resonating element 42 of the sensor 20 for tissue characterization, in accordance with the present invention,

As seen in Figure 3A and 3B, the resonating element 42 is formed as a flat spiral 22, of a conductive material, such as copper, gold, or another conductor, as known. An inner end 41 may be resistively connected to the coupler 50, via a conductive lead 43. However, a second end 47 may be free, so as to be inductively coupled to the circuit 40 (Figure 2A). Alternatively, the second end 47 may be connected to the coupler 50, while the first end 41 may be free.

The spiral 22 is associated with the equivalent diameter D.

As seen in Figure 3B, the spiral 22 may be deposited on a substrate 49, to a thickness of about 4 microns. It will be appreciated that other dimensions may similarly be used. The substrate may be, for example, polycarbon, quartz, or another material as known. The purpose of the substrate 49 is to prevent a response from a distal side of the spiral 22.

Preferably, an insulation layer 48, for example, Kapton, of about 4 microns, may be applied over the spiral 22. It will be appreciated that other dimensions may similarly be used.

The width d1 of the conductive material 45, and the spacing d2 are generally of the same order of magnitude, and are termed, the feature size. In general, these may influence the resolution capability of the sensor 20, and especially the special resolution and are preferably no more than half the size of the desired resolution capability. For example, when a minimal detectable object size of about 0.25 mm is sought, a feature size which is about of about 0.1 mm, being 40% of the desired resolution capability may be used.

Figure 3C illustrates the spiral 22, with both ends 41 and 47 resistively coupled to the circuit 40, via conductive leads 43.

Figure 3D illustrates a double spiral 22A, with the two inner ends 41 resistively coupled and the two outer ends 47, being free.

Figures 3E and 3F schematically illustrate a conical helix 24, which is similarly deposited on the substrate 49. However, the substrate 49 is shaped as a funnel, to provide the conductive material 45 with the cone shape.

The conical helix 24 is associated with the equivalent diameter  $D$  and with a length  $L$ . Additionally, it is associated with the width  $d1$  of the conductive material 45, and the spacing  $d2$ , as for the spiral 22. The conical helix 24 is shown resistively coupled. Alternatively, it may be inductively coupled.

5        Figures 3G – 3K schematically illustrate the resonating element 42, wherein the conductive material 45 is formed as two combs 45A and 45B, inserted into each other, as shown in Figures 3H and 3I, to form a structure 28.

      The conductive material 45 forming the structure 28 may be deposited on the insulating material 48, such as Kapton, of a thickness of about 100 microns, and  
10        covered with the insulating material 48, such as Kapton of a thickness of between about 4 and 50 microns.

      Contact points 55 provide resistive coupling to the structure 28.

      Preferably, the structure 28 is placed over a cavity 51, formed by a housing 53. The purpose of the cavity 51 being to prevent a response from a distal side of the  
15        structure 28.

      Referring further to the drawings, Figures 4A – 4C schematically illustrate the sensor 20, formed as a thin, flexible construction 75, in accordance with an embodiment of the present invention.

      Preferably, the sensor 20 includes the spiral 22, of a thickness of about 4  
20        microns, deposited on the insulating material 48, such as Kapton, of a thickness of about 100 microns, and covered with the insulating material 48, such as Kapton to a thickness of 50 microns, thus being essentially self-supporting.

      The flexible construction 75 is configured to bend at a line 77, so that in operation, the spiral 22 is substantially at a right angle to the remainder of the flexible  
25        construction 75. Additionally, the flexible construction 75 is adapted for operation when inserted into a hollow housing 74, having a top cover 57 of polycarbon, wherein the spiral 22 forms a proximal cover over the top cover 57 of polycarbon, for forming contact or near contact with the edge 13 of the tissue 18 (Figure 1). The hollow housing 74 essentially provides the effective cavity 51, at the distal side of the sensor  
30        22.

      Referring further to the drawings, Figures 5A – 5G, schematically illustrate the sensor 20 operative with a housing 70, in accordance with the present invention.

In accordance with the present embodiment, the sensor 20 may include the spiral 22 and a helix 26. These may be connected in series, or in parallel, as shown in Figure 2B. Additionally, either one may be resistively coupled or inductively coupled, so as to have one free end.

5 The housing 70 preferably includes an inner support structure 65, having a circular head 62 and a leg 64, so as to have a T-shaped cross section, and having proximal and distal ends 61 and 69, with respect to the tissue.

The spiral 22 is preferably positioned at the head 62. The helix 26 may be coiled around the leg 64. The leg 64 may further be used to house the conductive lead  
10 43 of the spiral 22.

Figure 5G schematically illustrates the coupler 50 having the connection structure 52 and the connector 54, at the distal end 69 of the housing 70.

Referring further to the drawings, Figures 6A – 6C schematically illustrate various manners of combining the spiral 22 and the helix 26, in accordance with the  
15 present invention.

In Figure 6A, the spiral 22 and the helix 26 are connected in parallel and both are inductively coupled.

In Figure 6B, the spiral 22 and the helix 26 are connected in series, and both are inductively coupled. It will be appreciated that a connection in series which is  
20 resistively coupled is also possible.

In Figure 6C, the spiral 22 and the helix 26 are connected in parallel and both are resistively coupled, via contacts 25.

Figure 7 schematically illustrates experimental data of the sensor for tissue characterization of the present invention, as obtained by the sensor 20 of Figures 4A-  
25 4C, having a diameter D of 7 mm. As seen in Figure 7, the resonating response of each of fibrosis, fatty tissue, and cancerous tissue has a different function of a reflection coefficient amplitude, as a function of wavelength, and may thus be identified based on its reflection coefficient amplitude, as a function of wavelength.

It is expected that during the life of this patent many relevant broad-band  
30 sensors, for tissue characterization will be developed and the scope of the term broad-band sensor, for tissue characterization is intended to include all such new technologies a priori.

As used herein the term "about" refers to  $\pm 20\%$ .

It is appreciated that certain features of the invention, which are, for clarity, described in the context of separate embodiments, may also be provided in combination in a single embodiment. Conversely, various features of the invention, which are, for brevity, described in the context of a single embodiment, may also be provided separately or in any suitable subcombination.

Although the invention has been described in conjunction with specific embodiments thereof, it is evident that many alternatives, modifications and variations will be apparent to those skilled in the art. Accordingly, it is intended to embrace all such alternatives, modifications and variations that fall within the spirit and broad scope of the appended claims.

All publications, patents and patent applications mentioned in this specification are herein incorporated in their entirety by reference into the specification, to the same extent as if each individual publication, patent or patent application was specifically and individually indicated to be incorporated herein by reference. In addition, any citation or identification of any reference in this application shall not be construed as an admission that such reference is available as prior art to the present invention.



**WHAT IS CLAIMED IS:**

1. A sensor for tissue characterization, comprising:

a resonating element, formed as a conductive structure, configured to be placed proximally to an edge of a tissue for characterization, without penetrating said tissue, and having a diameter-equivalent  $D$ , which defines a cross-sectional area of said resonating element, on a plane substantially parallel with said edge; and

at least one conductive lead, for providing communication with an external system,

wherein said resonating element is configured to resonate at a free-air wavelength range of between about  $\lambda$  and about  $10\lambda$ , wherein  $\lambda$  is at least about ten times said diameter-equivalent  $D$ ,

and wherein upon receiving a signal in said range of between about  $\lambda$  and about  $10\lambda$ , said sensor is configured to induce electric and magnetic fields, in a near zone, in said tissue, said near zone being substantially a hemisphere having a diameter of substantially  $D$ , beginning at said edge,

so that said tissue, in said hemisphere, effectively functions as part of said resonating element, varying a resonating response to said sensor,

and so said tissue, in said hemisphere, is thereby characterized by its electromagnetic properties, by said resonating response to said sensor.

2. The sensor of claim 1, wherein in a far zone, said sensor has a radiation efficiency of less than 0.1 %, for said free-air wavelength range of between about  $\lambda$  and about  $10\lambda$ .

3. The sensor of claim 1, and further including a connector to a transmission line, said connector providing substantial impedance matching between said sensor and said transmission line.

4. The sensor of claim 1, and further including a connection structure, associated with said connector, for providing a capability selected from the group consisting of a tuning capability, a switching capability, and a replacement capability,

to components of said connector, for interchangeably optimizing said sensor to different applications.

5. The sensor of claim 1, wherein said resonating element is formed as a substantially flat spiral.

6. The sensor of claim 1, wherein said resonating element is formed as two substantially flat spirals, wound together.

7. The sensor of any of claims 5 or 6, formed as a thin, flexible construction, adapted for operation when inserted into a hollow housing, wherein said resonating element bends to form a proximal top to said hollow housing.

8. The sensor of claim 1, wherein said resonating element is formed as a conical helix.

9. The sensor of claim 8, deposited on a funnel-shaped substrate.

10. The sensor of claim 1, wherein said resonating element is formed as two combs, inserted into each other.

11. The sensor of claim 1, wherein said resonating element is deposited over a self-supporting substrate.

12. The sensor of claim 1, wherein said resonating element is deposited over a thin substrate and placed over a housing which forms a cavity.

13. The sensor of claim 1, wherein said resonating element is formed of two parts, a substantially flat spiral and a helix.

14. The sensor of claim 13, wherein said two parts are connected in parallel.

15. The sensor of claim 13, wherein said two parts are connected in series.
16. The sensor of claim 1, wherein said resonating element is inductively coupled.
17. The sensor of claim 1, wherein said resonating element is resistively coupled.
18. The sensor of claim 1, wherein said D is between about 3 and about 25 mm.
19. The sensor of claim 1, designed with balancing.
20. The sensor of claim 1, sensitive to suspicious object sizes of about 0.25 mm in diameter and greater.
21. A system for tissue characterization, comprising:
  - a sensor for tissue characterization, which comprises:
    - a resonating element, formed as a conductive structure, configured to be placed proximally to an edge of a tissue for characterization, without penetrating said tissue, and having a diameter-equivalent D, which defines a cross-sectional area of said resonating element, on a plane substantially parallel with said edge; and
    - at least one conductive lead, for providing communication with an external signal-generation-control-and-analysis system,
    - wherein said resonating element is configured to resonate at a free-air wavelength range of between about  $\lambda$  and about  $10\lambda$ , wherein  $\lambda$  is at least about ten times said diameter-equivalent D,
    - and wherein upon receiving a signal in said range of between about  $\lambda$  and about  $10\lambda$ , said sensor is configured to induce electric and magnetic fields, in a near zone, in said tissue, said near zone being substantially a hemisphere having a diameter of substantially D, beginning at said edge,
    - so that said tissue, in said hemisphere, effectively functions as part of said resonating element, varying a resonating response to said sensor,

and so said tissue, in said hemisphere, is thereby characterized by its electromagnetic properties, by said resonating response to said sensor; and  
said external signal-generation-control-and-analysis system, in communication with said sensor, via said at least one conductive lead.

22. A method of tissue characterization, comprising:

providing a sensor for tissue characterization, which comprises:

a resonating element, formed as a conductive structure, configured to be placed proximally to an edge of a tissue for characterization, without penetrating said tissue, and having a diameter-equivalent  $D$ , which defines a cross-sectional area of said resonating element, on a plane substantially parallel with said edge; and

at least one conductive lead, for providing communication with an external system,

wherein said resonating element is configured to resonate at a free-air wavelength range of between about  $\lambda$  and about  $10\lambda$ , wherein  $\lambda$  is at least about ten times said diameter-equivalent  $D$ ,

and wherein upon receiving a signal in said range of between about  $\lambda$  and about  $10\lambda$ , said sensor is configured to induce electric and magnetic fields, in a near zone, in said tissue, said near zone being substantially a hemisphere having a diameter of substantially  $D$ , beginning at said edge,

so that said tissue, in said hemisphere, effectively functions as part of said resonating element, varying a resonating response to said sensor,

and so said tissue, in said hemisphere, is thereby characterized by its electromagnetic properties, by said resonating response to said sensor;

providing said sensor with sweeping signals within said range of between about  $\lambda$  and about  $10\lambda$ , thus inducing electric and magnetic fields, in said near zone, in said tissue;

recording said resonating response to said sensor, as a function of said sweeping signals; and

characterizing said tissue by said resonating response.

**ABSTRACT OF THE DISCLOSURE**

A sensor for tissue characterization is provided, comprising: a resonating element, formed as a conductive structure, configured to be placed proximally to an edge of a tissue for characterization, without penetrating the tissue, and having a diameter-equivalent  $D$ , which defines a cross-sectional area of the resonating element, on a plane substantially parallel with the edge; and at least one conductive lead, for providing communication with an external system, wherein the resonating element is configured to resonate at a free-air wavelength range of between about  $\lambda$  and about  $10\lambda$ , wherein  $\lambda$  is at least about ten times the diameter-equivalent  $D$ , and wherein upon receiving a signal in the range of between about  $\lambda$  and about  $10\lambda$ , the sensor is configured to induce electric and magnetic fields, in a near zone, in the tissue, the near zone being a hemisphere having a diameter of substantially  $D$ , beginning with the edge, while causing negligible radiation in a far zone, so that the tissue, in the near zone, effectively functions as part of the resonating element, varying a resonating response to the sensor, and so the tissue, in the near zone, is thereby characterized by its electromagnetic properties, by the resonating response to the sensor.

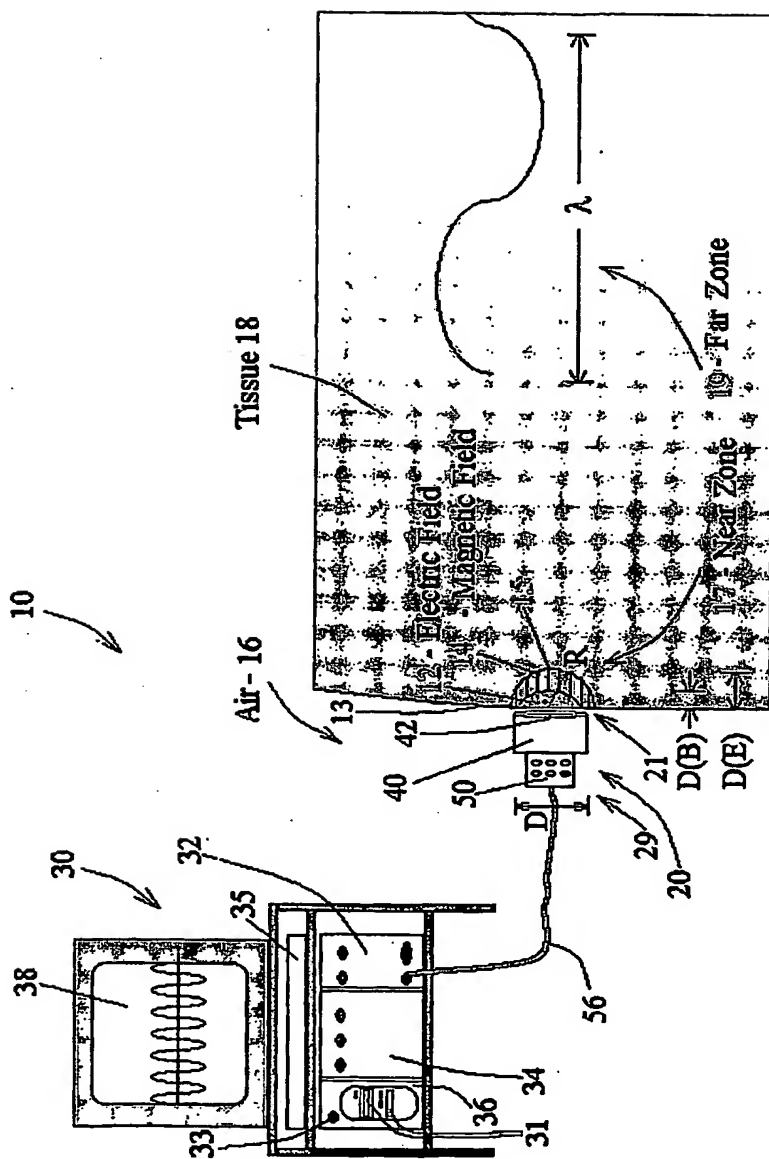


Figure 1

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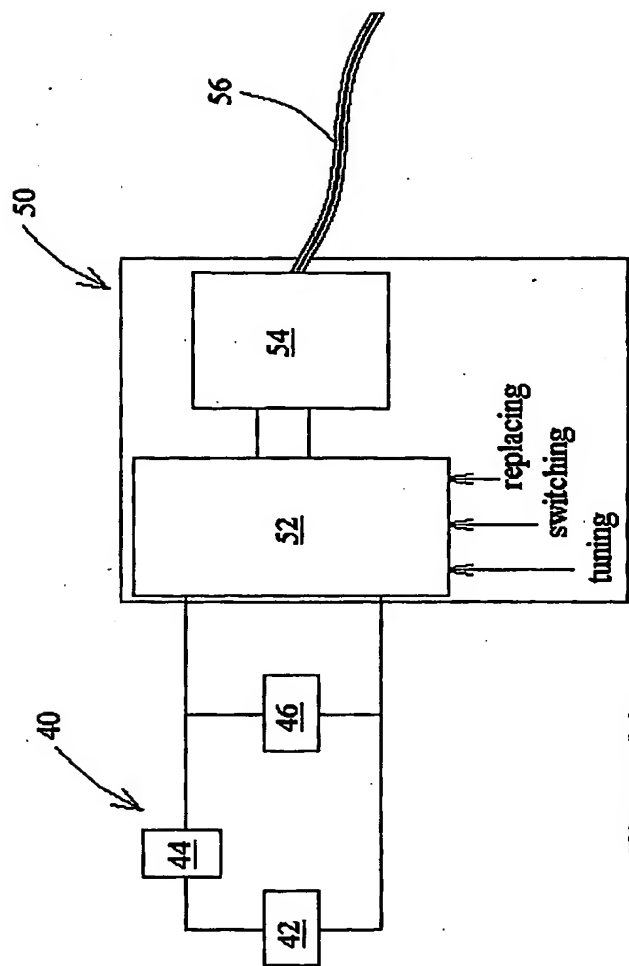


Figure 2A

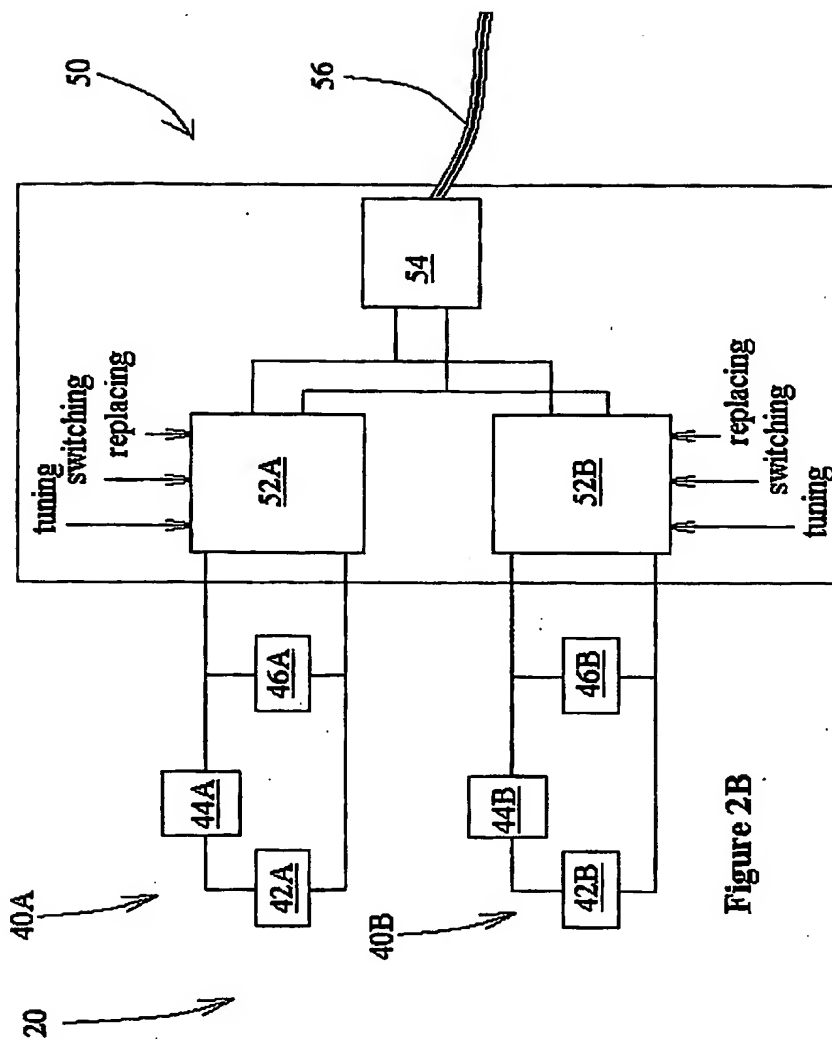


Figure 2B



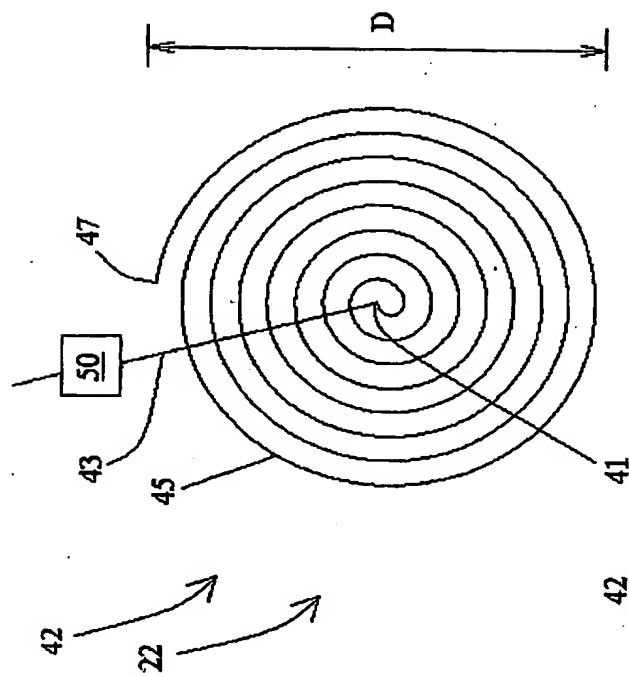


Figure 3A

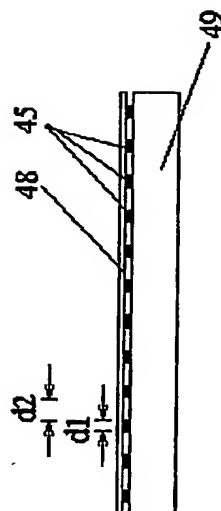


Figure 3B

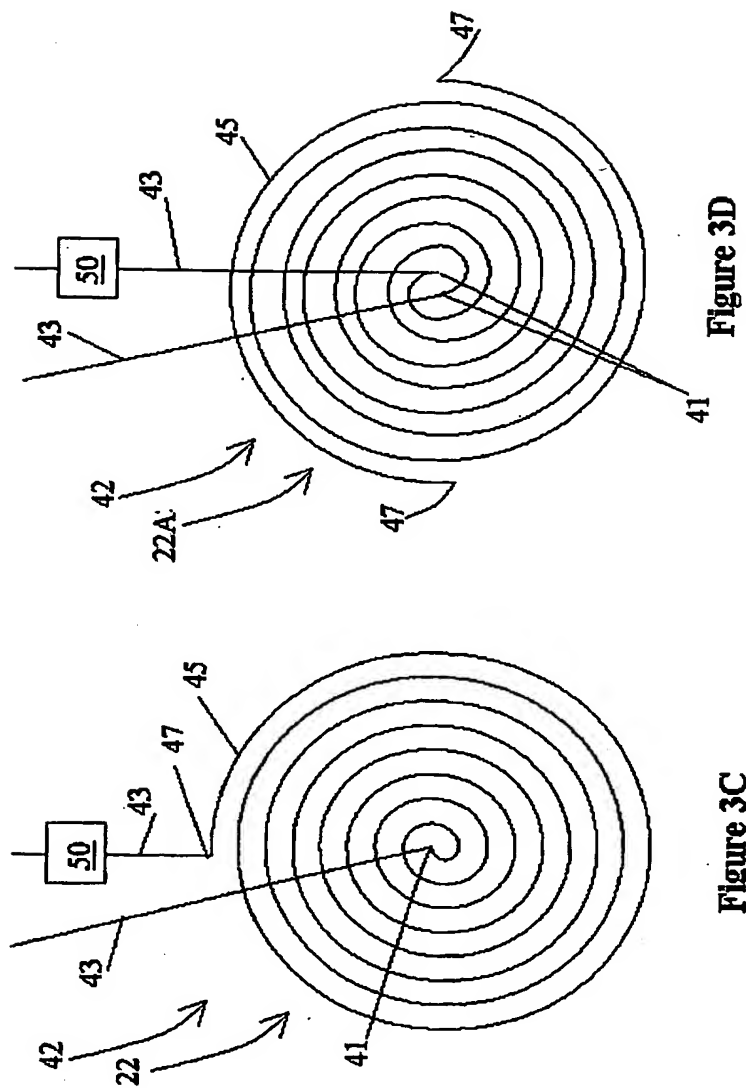


Figure 3D

Figure 3C

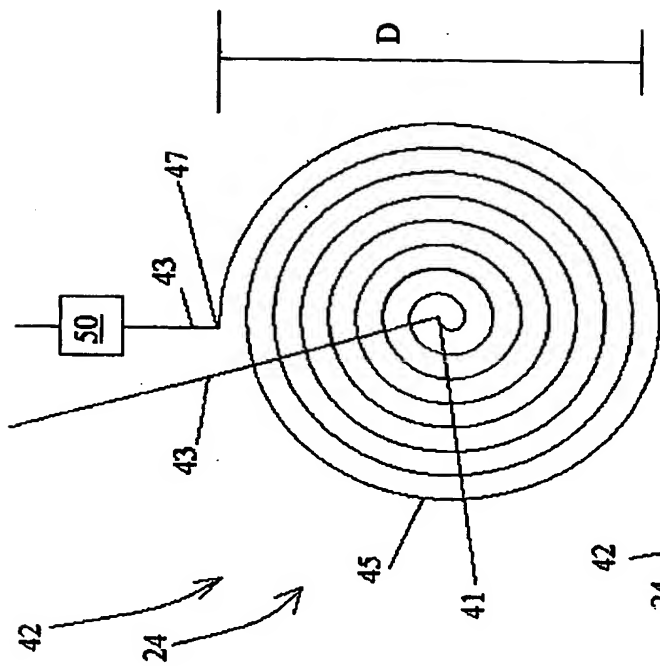


Figure 3E

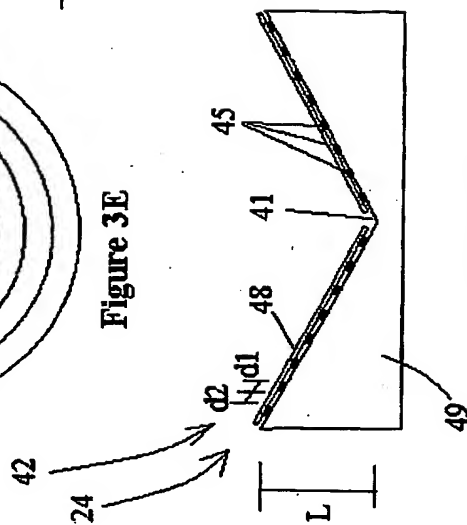
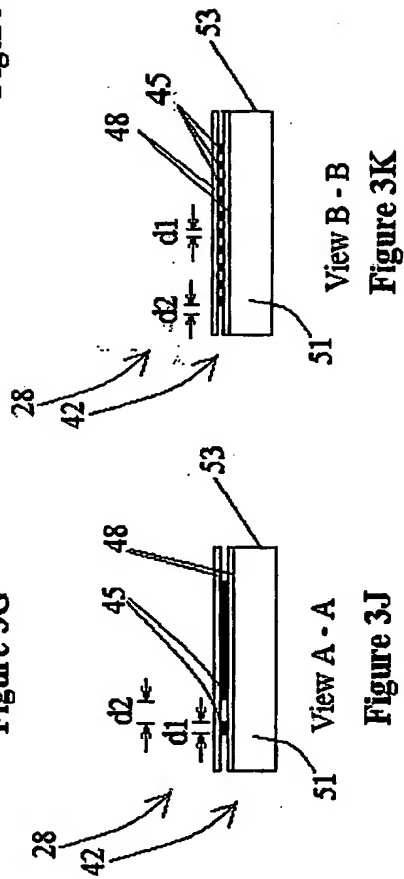
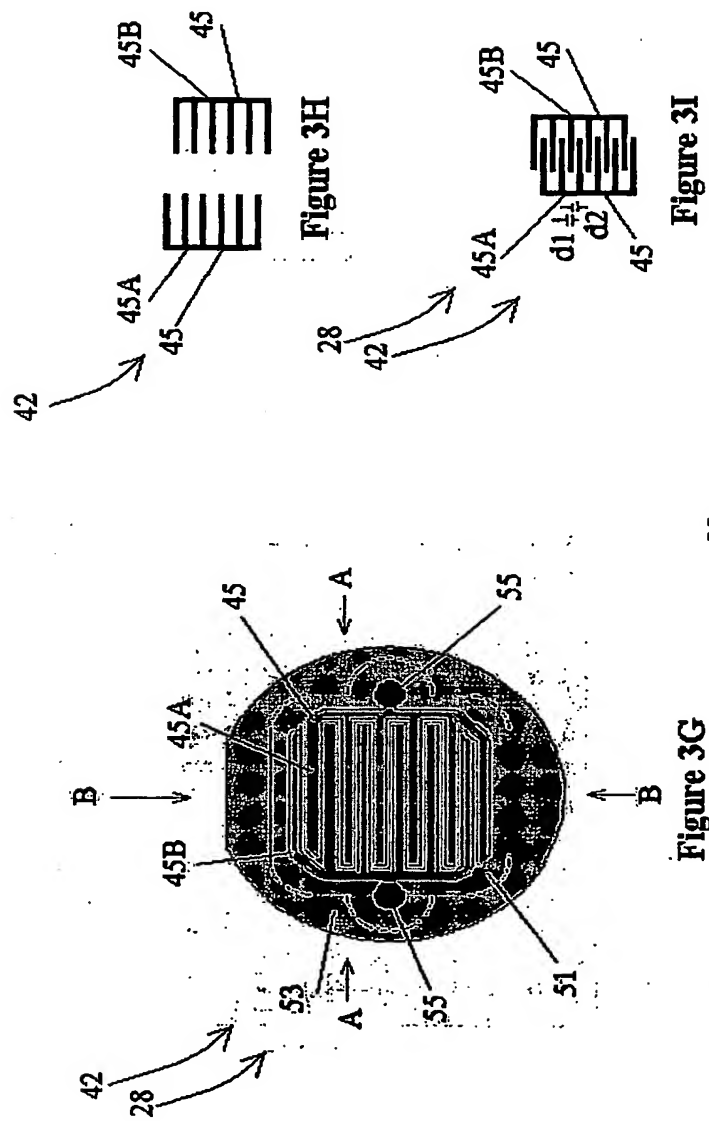


Figure 3F



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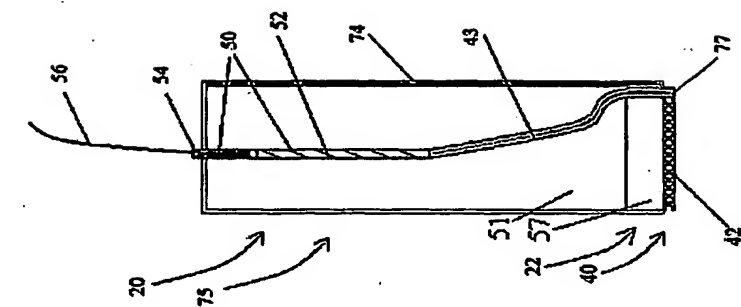


Figure 4C

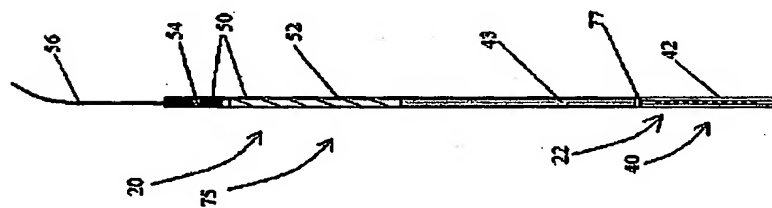


Figure 4B

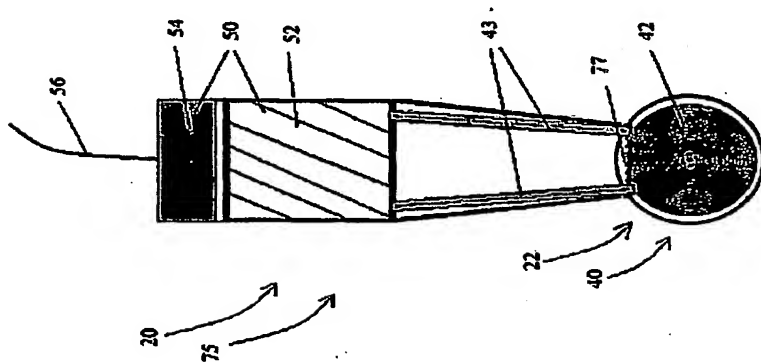


Figure 4A

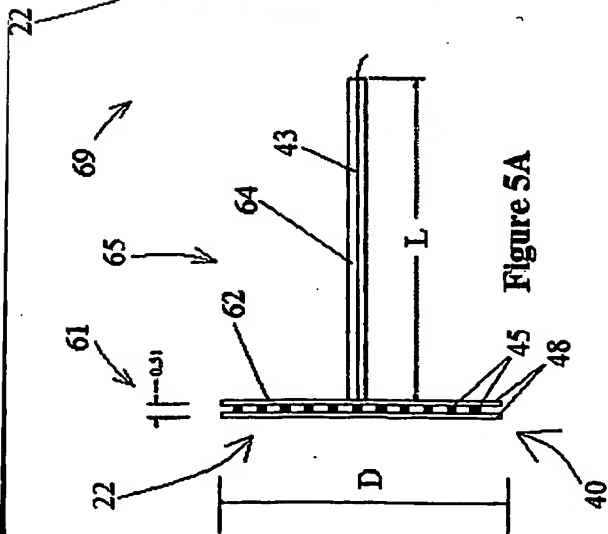


Figure 5A

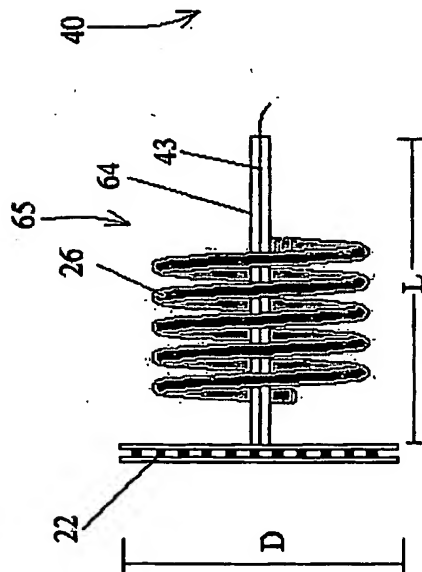


Figure 5C

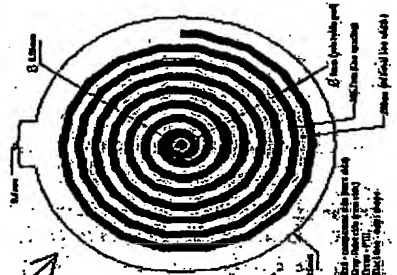


Figure 5B

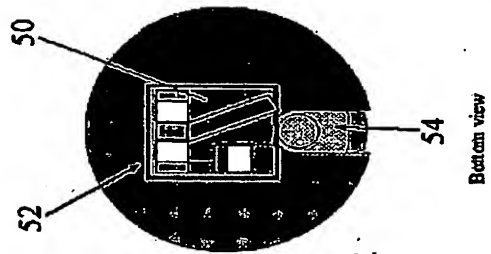


Figure 5G

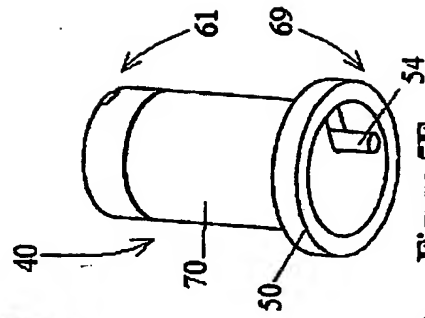


Figure 5F

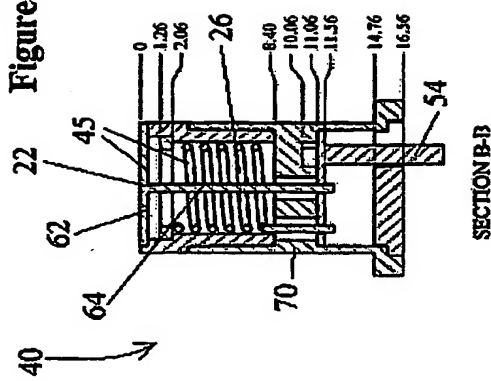


Figure 5E

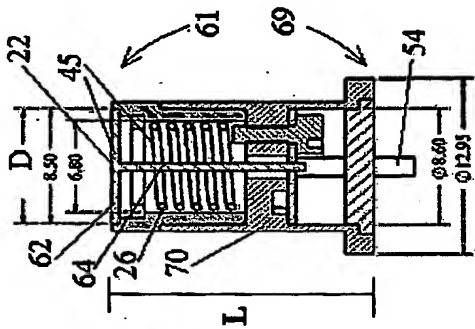


Figure 5D

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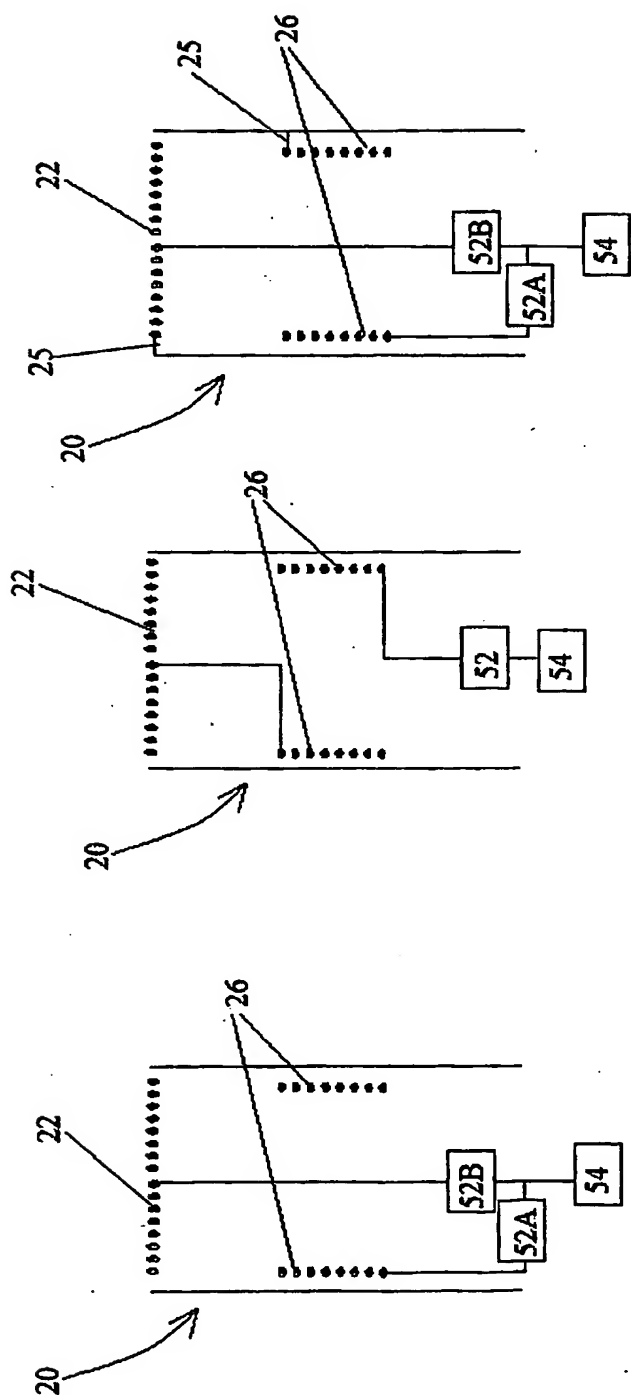


Figure 6C

Figure 6B

Figure 6A

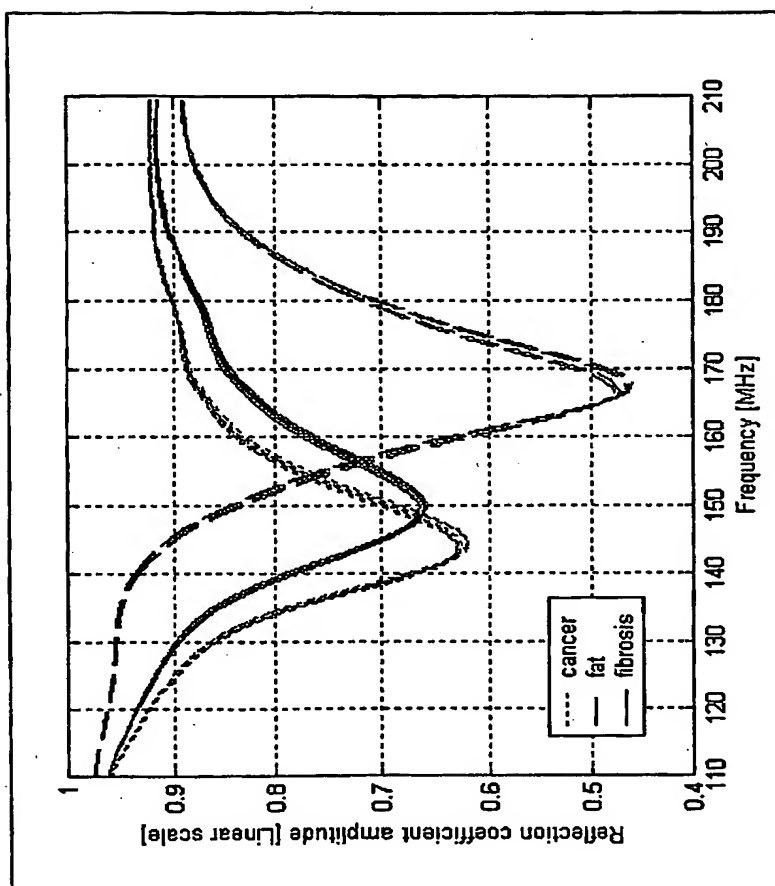


Figure 7